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(54) **HIGH-SPEED SPECTROGRAPHIC SENSOR
FOR INTERNAL COMBUSTION ENGINES**

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G01B 9/02 (2006.01)

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(58) **Field of Classification Search** **356/451,**
356/320, 450

See application file for complete search history.

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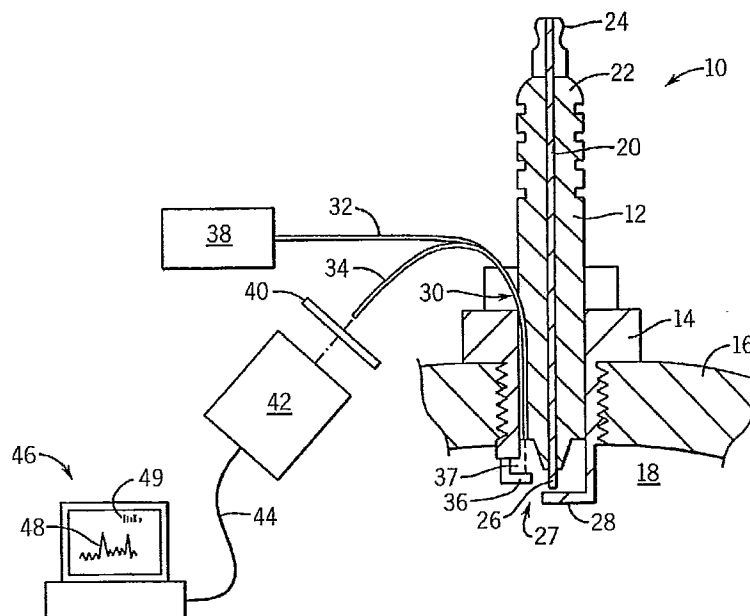
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ABSTRACT

A high-speed absorption spectrographic system employs a
slit-less spectroscope to obtain high-resolution, high-speed
spectrographic data of combustion gases in an internal com-
bustion engine allowing precise measurement of gas param-
eters including temperature and species concentration.

21 Claims, 2 Drawing Sheets



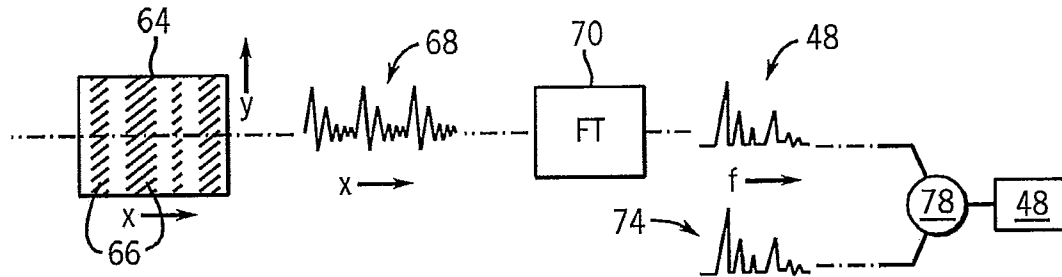


FIG. 3

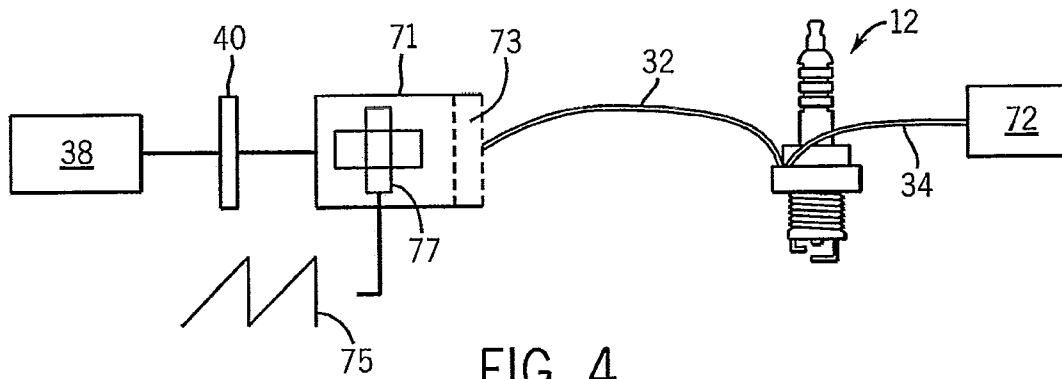


FIG. 4

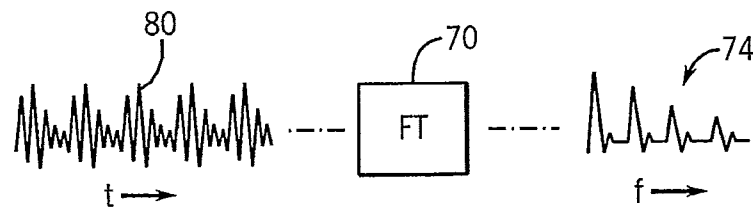


FIG. 5

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It is thus another aspect of at least one embodiment of the invention to provide for measurement in the vicinity of the spark in operating the internal combustion engine.

These particular objects and advantages may apply to only some embodiments falling within the claims and thus do not define the scope of the invention.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a cross-sectional view of a modified spark plug holding a light guide for receiving light to interact with combustion gases and transmitting the light back to a spectro-
scope for high-speed analysis;

FIG. 2 is a block diagram of a spatial heterodyne spectrometer suitable for use as the spectroscopy of FIG. 1;

FIG. 3 is a diagram of the process steps of converting an image from the spatial heterodyne spectrometer into a spectrum and in performing signature matching;

FIG. 4 is a block diagram of the alternative embodiment of the invention using the spark plug of FIG. 1 but employing a Fourier spectrometer upstream from the spark plug; and

FIG. 5 is a figure similar to that of FIG. 3 showing those steps of signal analysis in the embodiment of FIG. 4 that differ from the embodiment of FIG. 1.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

Referring now to FIG. 1, a high-speed spectrographic sensor 10 of the present invention provides for a modified spark plug 12 that may be fit to a combustion chamber 18. In the manner of conventional spark plugs, the spark plug 12 may provide a conductive threaded flange 14 fitting within a corresponding threaded bore in the wall 16 of the combustion chamber 18, providing a seal therewith.

The spark plug 12 provides a center electrode 20 coaxially within a ceramic insulator 22 and passing from outside of the chamber 18 where it is accessible at a high-voltage terminal 24 to inside the chamber 18 where it extends out of the insulator 22 as an electrode tip 26. A ground electrode 28 extends from the flange 14 into the combustion chamber 18 to a point opposite the electrode tip 26 across a spark gap 27 in a manner known in the art.

The insulator 22 or threaded flange 14 also holds a light guide 30 passing through the insulator 22 or threaded flange 14 from outside the combustion chamber 18 to a point within the combustion chamber 18 near the spark gap 27. The light guide 30 may be, in a preferred embodiment, two adjacent optical fibers 32 and 34, one for carrying light into the combustion chamber 18 and one for carrying light out of the combustion chamber 18 for sensing.

The fiber 32 carrying the light into the combustion chamber 18 may receive light from a broad spectrum light source, such as an incandescent bulb in the form of a quartz tungsten-halogen lamp, or a wideband LED or broadband laser, providing substantial energy in the range of 2000 nm to 3000 nm and preferably in a range of 2400 nm to 2600 nm and having a known spectrum.

A mirror 36 is positioned across a gap 37 from the point where the light guide 30 terminates in the combustion chamber 18. The mirror 36 is positioned so that light passing through optical fiber 32 exits the light guide 30 and passes across the gap 37 to strike the mirror 36, to be reflected back across the gap 37 and be received by fiber 34. The optical path through the gap 37 may be as great as 10 mm to allow the light to interact with combustion gases in the region of the electrode tip 26.

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Light received from optical fiber 34, after interacting with the combustion gases, passes through a filter 40, for example, a band limiting filter of the desired frequency range (e.g. 2400-2600 nm). The filtered light is then received by a spectrometer 42 which in the preferred embodiment is a spatial heterodyne spectrometer.

The spectrometer 42 provides a digitized output 44 received by a computer 46. The computer executes a program to display a high-resolution absorption spectrum 48 (based on known or measured spectrum of light source 38) extracted every 100 μ s and no less than every 1000 μ s and consisting of hundreds of resolved frequency points and no less than twenty resolved frequency points. The computer 46, operating according to the stored program, may also identify a quantitative parameter value 49, being for example a temperature of the combustion gases or a species mole fraction such as water concentration or other similar measurement, as will be described.

Referring now to FIG. 2, the spatial heterodyne spectrometer 42 provides an open aperture and high-speed response made possible by its efficient use of minor energy obtained through fiber 34. Spectrometers of this type are described in U.S. Pat. No. 5,059,027, issuing Oct. 22, 1991, assigned to the assignee of the present invention, and hereby incorporated by reference. Such a spectrometer receives a light signal 50 from the fiber 34 and collimates this light using an optical assembly 52 to provide for a beam 53 having generally an aligned wavefront 54.

A dispersive optical system 56 tips the wavefronts 55 of each of multiple frequency component in the light signal 50 (only two shown) to an angle α dependent on the wavelength of that frequency component. The wavefront-modified beam 58 is then received by an imaging optical assembly 60 to project an image on a solid-state image detector 62 such as an extended InGaAs line scan camera commercially available from Xenics Leuven, Belgium. The signal from the solid-state image detector 62 may be digitized and sampled per block 63 to produce an image 64 at approximately 1000 times per second or as much as 10,000 times per second.

Referring now also to FIG. 3, the image 64 from the solid-state image detector 62 will contain a series of bands of different intensities 66 caused by interference in the image produced by the constructive and destructive interference of the wavefronts 55 as tipped by dispersive optical system 56. The information of this image 64 may be collapsed to a single dimension (x) to produce a spatially dependent signal 68 with improved signal-to-noise ratio that better utilizes all of light energy from the fiber 34 both improving the speed and the resolving power of the spectrum.

This signal 68, when operated on by the Fourier transform 70, as may be implemented in the computer 46 of FIG. 1, produces a high-resolution spectrum 48 providing resolvable points for more than 100 different frequencies. The high-resolution spectrum 48 may be compared to spectrum 74 of a library 76 of different signature spectra 74 by a correlator 78, where each signature spectra 74 is associated with a known physical parameter that is to be extracted. For example, the multiple spectra 74 may each represent measurements of combustion gases at a different temperature. Alternatively the multiple spectra 74 may each represent a measurement of a different water concentration or another species concentration.

The correlator 78 finds the best correlation between high-resolution spectrum 48 and each of spectra 74 to output a measured temperature or other quantitative parameter value 49 as shown in FIG. 1, according to the parameter associated with the most highly correlated spectra 74.

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- (b) introducing light at multiple frequencies having wavelengths less than 3000 nm into the light guide to interact with combustion gases; and
- (c) receiving light from the plug through the light guide at a slit-less spectroscopy attached to the light guide to receive light from the light guide directly also without an intervening slit;
- (d) spatially separating multiple light frequencies as received simultaneously by an optical system of the spectroscopy after passage through the combustion chamber to permit simultaneous monitoring of the multiple frequencies at different spatial locations; the spectroscopy distinguishing strength of no less than 20 multiple frequencies of the light at a rate of no less than 1000 times per second after interaction with the combustion gases.
13. The method of claim 12 wherein the determining spatially heterodynes the light received after interaction with the combustion gases to determine attenuation of the multiple frequencies.
14. The method of claim 12 further including outputting temperature within the combustion chamber from the strengths of the multiple frequencies.
15. The method of claim 12 further including outputting water concentration within the combustion chamber from the strengths of the multiple frequencies.

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16. The method of claim 12 further including matching the strength of the multiple frequencies to multiple signatures with similar multiple frequencies and representing known different physical parameters to deduce a physical parameter within the combustion chamber.
17. The method of claim 12 wherein the light includes frequencies having wavelengths substantially within a range of 2400-2600 nm.
18. The method of claim 12 wherein the attenuation of no less than 100 multiple frequencies is determined.
19. The method of claim 12 wherein the attenuation of the multiple frequencies is determined no less than 10,000 times a second.
20. The method of claim 12 further including measuring and time-modulating the multiple frequencies before the light interacts with the combustion gases; and demodulating a time signal derived from a strength of the multiple frequencies to distinguish the strength among the multiple frequencies after interaction with the combustion gases.
21. The method of claim 12 further including providing an ignition spark in the vicinity of the light guide within the combustion chamber.

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